

Efficient on-the-fly Operator Assembly for HPC Finite **Element Codes**

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Software Framework - Hierarchical Hybrid Grids (HHG) [1]

- · Unstructured macro mesh
- Uniform refinement of macro elements
- Primitive based data structures + ghost laver exchange
- · Matrix-free implementation (on-the-fly stencil assembly)

Problem: On-the-fly stencil assembly on curved domains requires expensive evaluation of local element matrices over and over again.



LSQP LocEL for Stokes-type PDE with variable viscosity - Performance Results on SuperMUC Phase1

Optimization Steps



DOFs using 1920 cores

A) standard on-the-fly FE stencil assembly

B) LSQP LocEl C) B + store stencils on lower dimensional primitives (faces)

D) C + optimized polynomial evaluation

LSQP LocEl 16x faster than standard FE assembly



Optimized memory usage with tuned MPI buffer sizes

_SEND_BUFFER_NUM=8208 _RECV_BUFFER_NUM=8208 _ACK_SEND_POOL_SIZE=8704 _ACK_RECV_POOL_SIZE=8704 _RNDV_EP_NUM=2

Avg. velocity whole mantle

Avg. velocity asthenosphere

Avg. velocity lower mantle

Max velocity lower mantle

Max velocity asthenosphere

References



Excludes all initialization times Only moderate increase of MPI communication. Most of the execution time is spent in comsmoothing pute-intense kernel

> ul 30.0 20.0 10.0 0.0

2.92 [cm/a]

7.02 [cm/a]

2.10 [cm/a]

42.46 [cm/a]

12.40 [cm/a]



Excellent parallel efficiency of more than 90% on up to 47 250 compute cores

Velocity streamlines at Iceland plume

Accuracy: Standard on-the-fly FE stencil assembly

Average velocities differ by less than 3% and

maximal velocities by even less than 1%

Geophysical Application at Extreme Scale - Global Resolution of ~ 1.7 km

Governing equations

cknowledgements

$$-\operatorname{div}(2\mu\dot{\varepsilon}(\mathbf{u})) + \nabla p = -\rho \mathbf{g}$$

 $\operatorname{div} \mathbf{u} = 0$

· Temperature dependent viscosity profile with jump at 660km depth (assumed to be bottom end of the asthenosphere)

$$\mu(\mathbf{x}, T) = \exp\left(4.61 \frac{1 - \|\mathbf{x}\|_2}{1 - r_{\rm cmb}} - 2.99T\right) \begin{cases} 1/10 \cdot 6.371^3 d_0^3 & \text{ for } \|\mathbf{x}\|_2 > 1 - d_a, \\ 1 & \text{ else.} \end{cases}$$

- Present day temperature and density field [3,4]
- Platevelocities [5] at surface and freeslip boundary conditions at core mantle boundary (cmb)
- Global 1.7km resolution yields system with O(1012) DOFs

Replace each component of 15pt stencil by a quadratic polynomial. Compute polynomial coefficients in setup phase by least-squares fit. Do this for each macro element.

verv fast

Novel Approach - FE Stencil Approximation

+ accuracy is O(h²) + O(H³) (for linear FE with element length h and macro element length H)

LSQP (least-squares polynomial) [2]

for PDEs with a variable material parameter this is only applicable, if the parameter is sufficiently smooth

Extension for PDEs with variable material parameter LSQP LocEl (local elements)



Replace entries of local element matrices by polynomial approximations. Use these approximations and the material parameter to assemble the stencils in a standard way. requires more FLOPs than LSQP, but still much faster than

- computing local element matrices via quadrature rules technique is applicable to PDEs with general material
- parameters

References
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vs. LSQP LocEl

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- - + for constant material parameter it is equivalent to LSQP